



Converting a Shake Table for Hybrid Simulation



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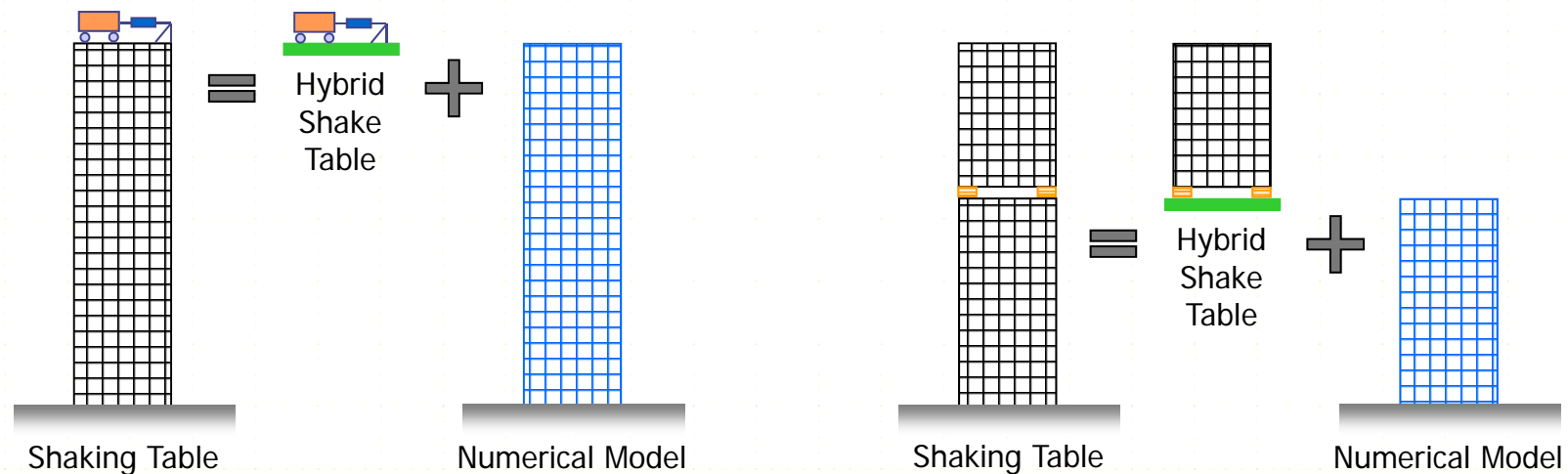


Outline of Presentation

1. Motivation
2. Hybrid Shake Table Testing
3. Stability and Accuracy Considerations
4. Test Rehearsal and Safety Precautions
5. Building Application
6. Summary & Conclusions

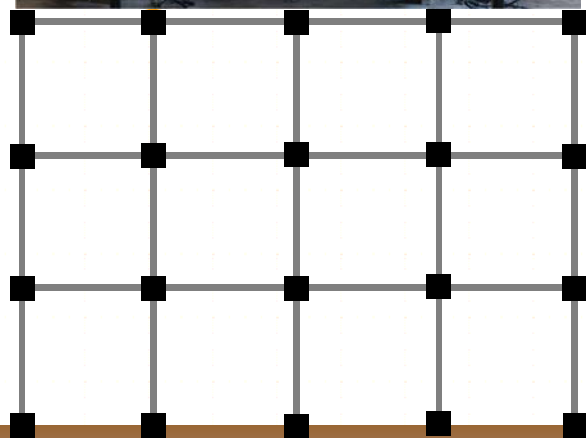
Motivation

- ★ Many structures exhibit significant rate of loading effects
- ★ Need testing to occur at or near real time
- ★ Large systems such as tall buildings, long-span bridges, or SFSI are difficult to test on shake tables

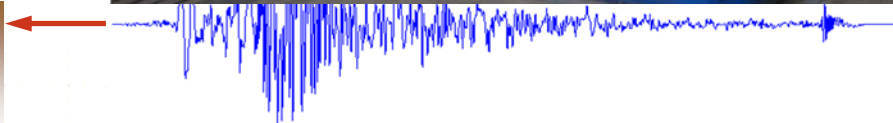


Hybrid Shake Table Testing

$$\mathbf{M} \cdot \ddot{\mathbf{u}} + \mathbf{C} \cdot \dot{\mathbf{u}} + \mathbf{P}_r(\mathbf{u}, \dot{\mathbf{u}}, \ddot{\mathbf{u}}) = \mathbf{P}(t)$$

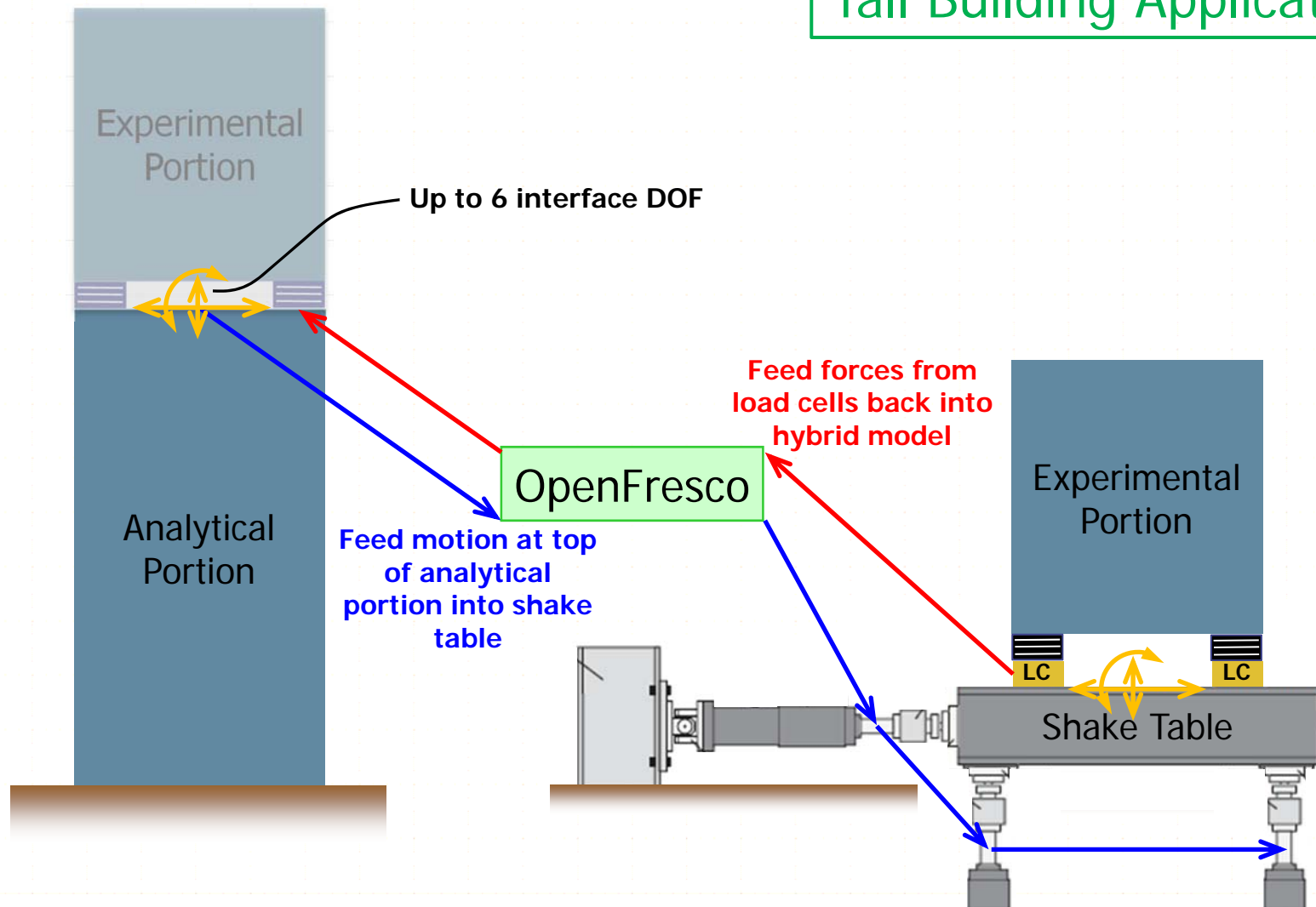


- ★ Inertia
- ★ Energy Dissipation
- ★ Resistance



Hybrid Shake Table Configuration

Tall Building Application



Equations of Motion

1. Slow test

$$\mathbf{M}\ddot{\mathbf{U}}_{i+1} + \mathbf{C}\dot{\mathbf{U}}_{i+1} + \mathbf{P}_r^A(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}) + \mathbf{P}_r^E(\mathbf{U}_{i+1}) = \mathbf{P}_{i+1} - \mathbf{P}_{0,i+1}$$

2. Rapid test

$$\mathbf{P}_r^E(\mathbf{U}_{i+1}) = \mathbf{P}_{r,i+1}^E - \mathbf{M}^E \ddot{\mathbf{U}}_{i+1}^E - \mathbf{C}^E \dot{\mathbf{U}}_{i+1}^E$$

3. Real-time test

$$\mathbf{M}^A \ddot{\mathbf{U}}_{i+1} + \mathbf{C}^A \dot{\mathbf{U}}_{i+1} + \mathbf{P}_r^A(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}) + \mathbf{P}_r^E(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}, \ddot{\mathbf{U}}_{i+1}) = \mathbf{P}_{i+1} - \mathbf{P}_{0,i+1}$$

$$\mathbf{P}_r^E(\mathbf{U}_{i+1}, \dot{\mathbf{U}}_{i+1}, \ddot{\mathbf{U}}_{i+1}) = \mathbf{P}_{r,i+1}^E + \mathbf{M}^E \ddot{\mathbf{U}}_{i+1}$$

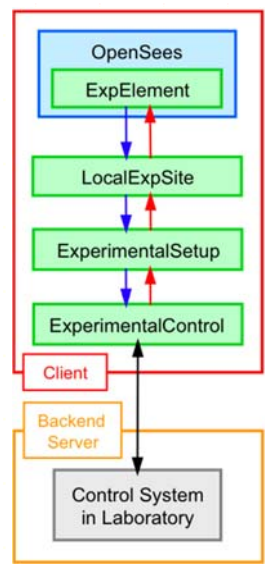
4. Smart shaking table test

$$\mathbf{P}_r^E(\mathbf{U}_{t,i+1}, \dot{\mathbf{U}}_{t,i+1}, \ddot{\mathbf{U}}_{t,i+1}) = \mathbf{P}_{r,i+1}^E + \mathbf{M}^E \ddot{\mathbf{U}}_{t,i+1}$$

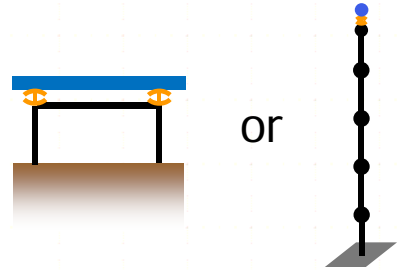
Important Analysis Parameters

- ★ OpenSees or OpenSees`SP` as comp. driver
- ★ Using AlphaOSGeneralized or KRAAlphaExplicit ($\rho_{inf} < 1.0$)
- ★ No iterations necessary
- ★ Using MultipleSupport excitation pattern in OpenSees to get `absolute` response
- ★ Gravity loads on test specimen always present → apply gravity loads to numerical portion `before` connecting with shake table + apply disp. commands relative to start of test

Connecting to MTS 469D & FlexTest



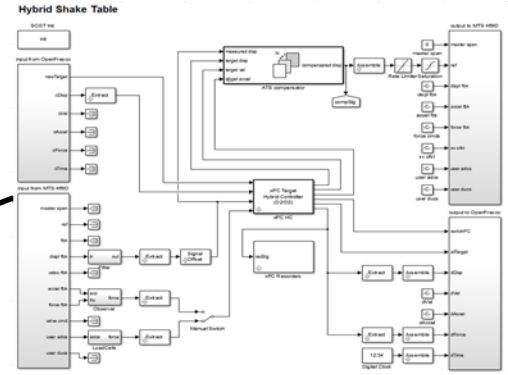
OpenSees Finite Element Model



OpenFresco Middleware

TCP/IP or SCRAMNetGT

xPC-Target real-time Predictor-Corrector



SCRAMNetGT

SCRAMNetGT

MTS 469D Controller

MTS FlexTest Controller



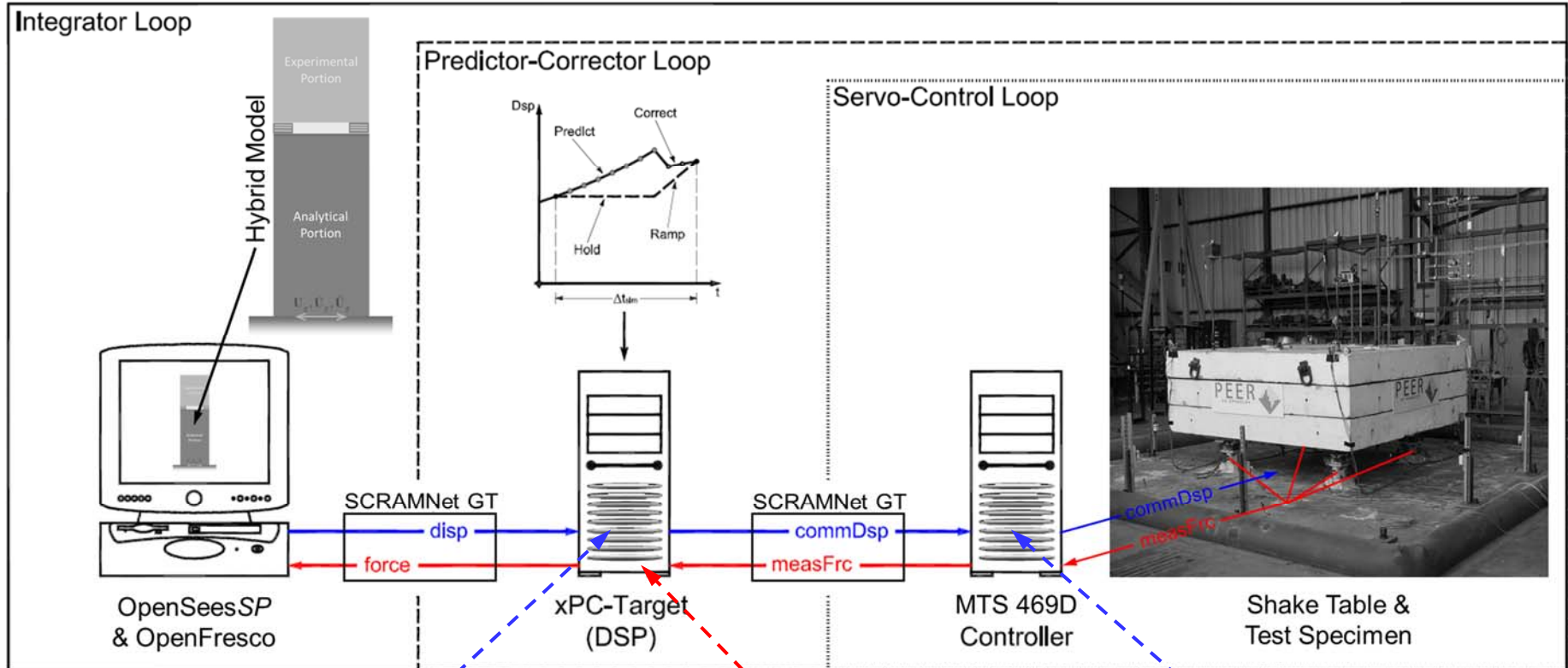
Physical Specimen in Laboratory



Improving Stability & Accuracy

- ★ Delay compensation is essential for real-time hybrid simulations (RTHS)
- ★ Use Adaptive Time Series (ATS) delay compensator (by Y. Chae)
- ★ Modify ATS to use target velocities and accelerations computed by predictor-corrector algorithm instead of taking derivatives of target displacements
- ★ Use stabilization and loop-shaping
- ★ Sensor noise reduction by filtering fbk

Three-loop architecture



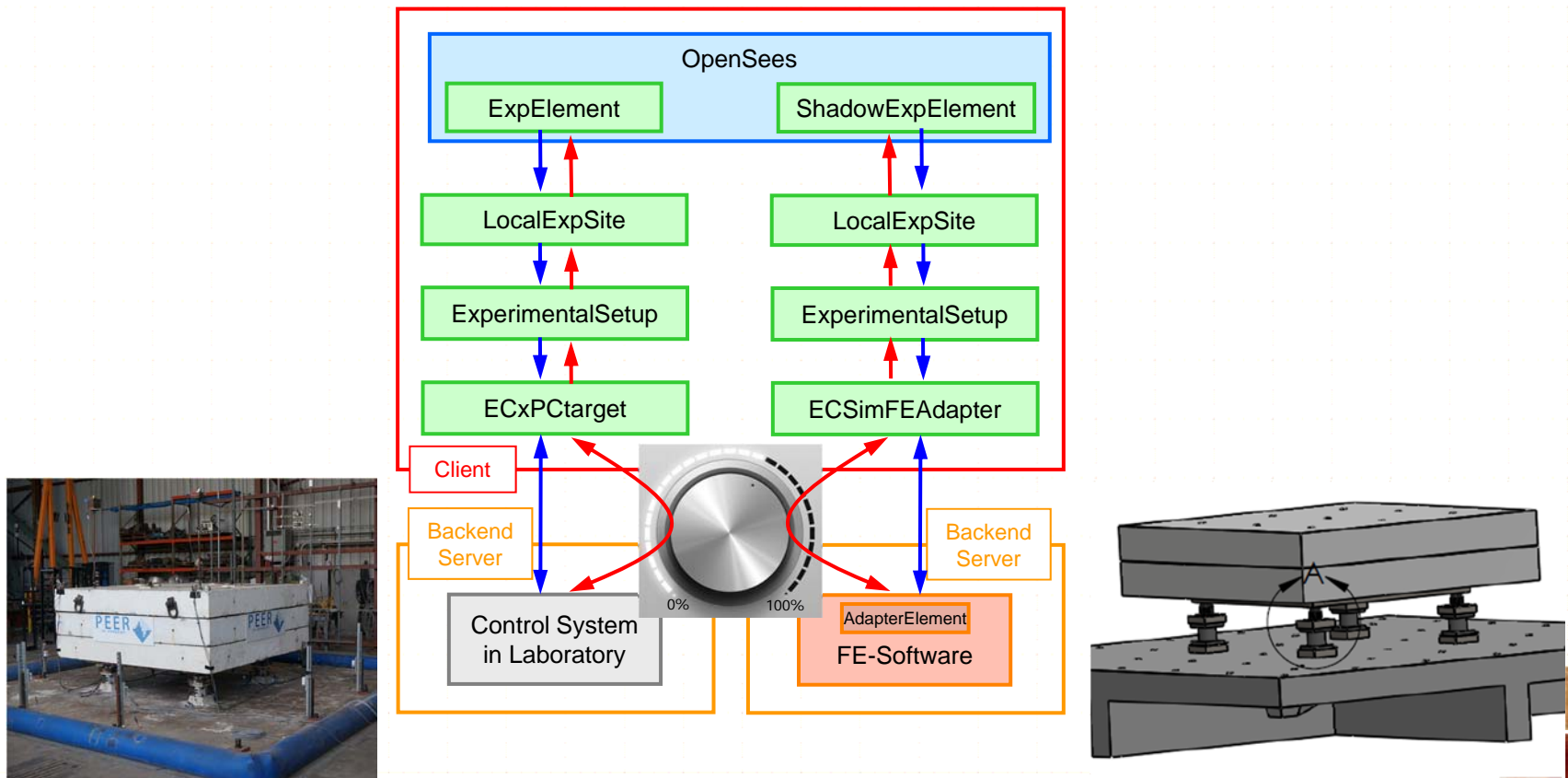
ATS delay
compensator

filtering &
noise reduction

TVC or other
adv. ctrl. &
force balancing

Test Rehearsal

- ★ Use FE-Adapter element method to simultaneously connect hybrid model to a numerically simulated test specimen



Safety Precautions

★ At analysis side

- Set limit on displacement command (saturation and possibly rate limit)
- Set limit on actuator force so that once the limit is exceeded, the analysis model sends displacement commands to ramp both table and actuator to starting positions

★ At controller side

- Set both displacement and force limits so that once the limit is exceeded, the actuator pressure is switched to low, therefore, limiting the actuator force that can be applied to the specimen

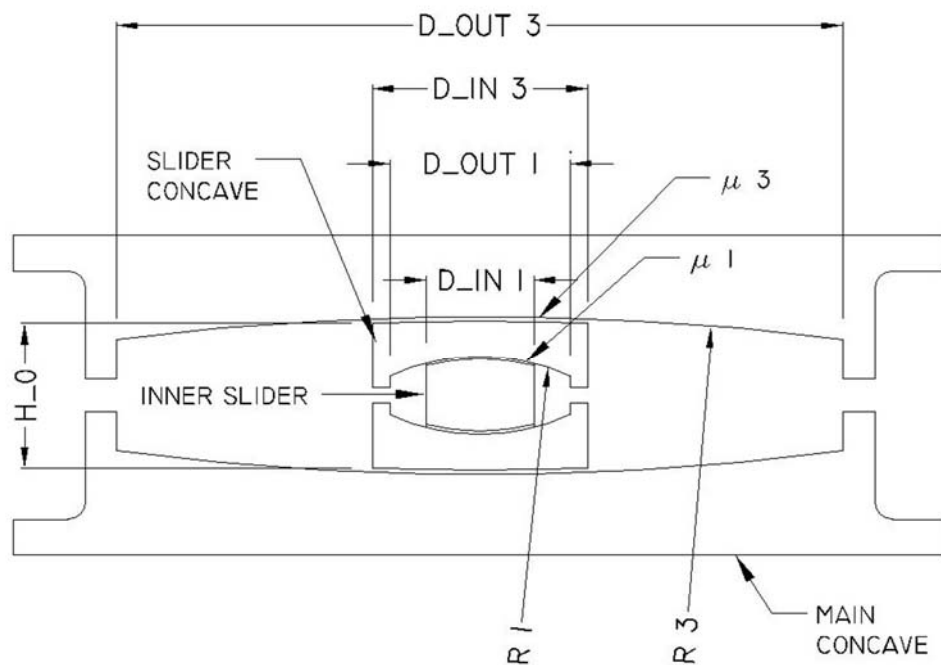
Building Application



6DOF Shake Table

LoadCells or
Observer to
get interface
forces

Triple Friction Pendulum Bearings



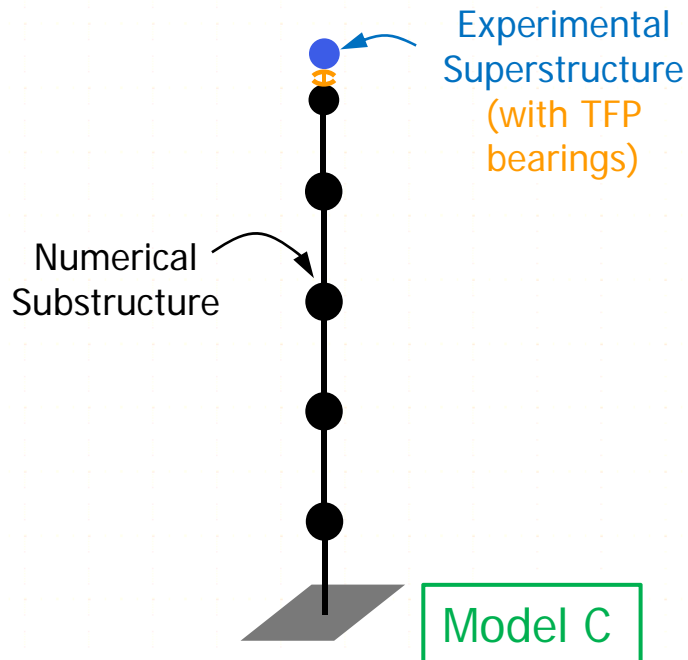
L1 (in.)	L2 (in.)	L3 (in.)
2.175	17.17	17.17

T1 (s)	T2 (s)	T3 (s)
0.67	1.41	1.87

	Inner sliding surfaces	Outer sliding surfaces
Dish radius (inch)	3	18.64
Height (inch)	1.65	2.94
Outer diameter (inch)	2.60	9
Inner diameter (inch)	1.75	3

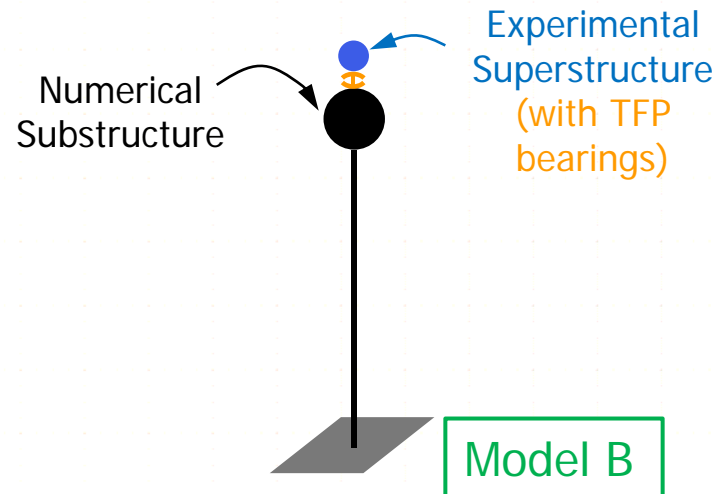
Analytical Substructure Parameters

Models without rotational DOF



15-DOF Shear Building

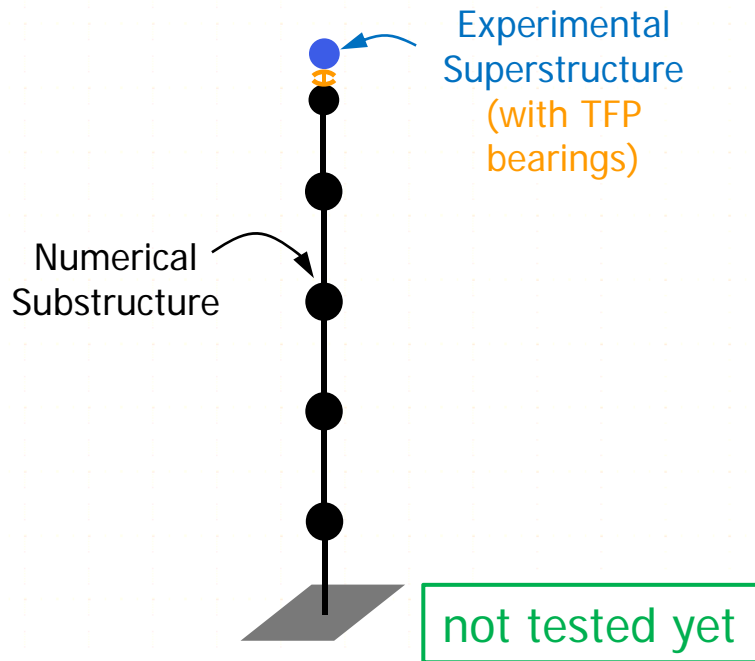
$$W_{\text{tmd}} = 53 \text{ kip}$$
$$W_{\text{bldg}} = 450 \text{ kip}$$
$$f_{x1} = 1 \text{ Hz}$$
$$f_{y1} = 1.25 \text{ Hz}$$
$$f_{z1} = 9.8 \text{ Hz}$$



3-DOF Equivalent Model

$$W_{\text{tmd}} = 53 \text{ kip}$$
$$W_{\text{bldg}} = 0.886 * 450 \text{ kip}$$
$$f_{x1} = 1 \text{ Hz}$$
$$f_{y1} = 1.25 \text{ Hz}$$
$$f_{z1} = 11 \text{ Hz}$$

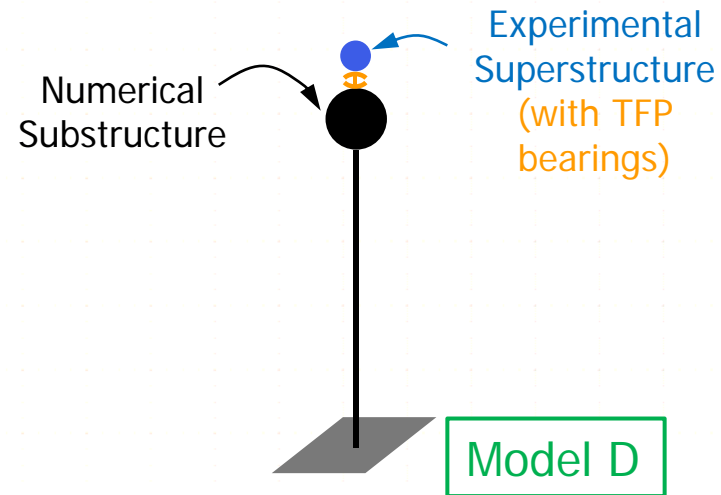
Analytical Substructure Parameters



30-DOF Flexural Building

$$W_{\text{tmd}} = 53 \text{ kip}$$
$$W_{\text{bldg}} = 450 \text{ kip}$$
$$f_{x1} = 1 \text{ Hz}$$
$$f_{y1} = 1.25 \text{ Hz}$$
$$f_{z1} = 9.8 \text{ Hz}$$

Models with rotational DOF

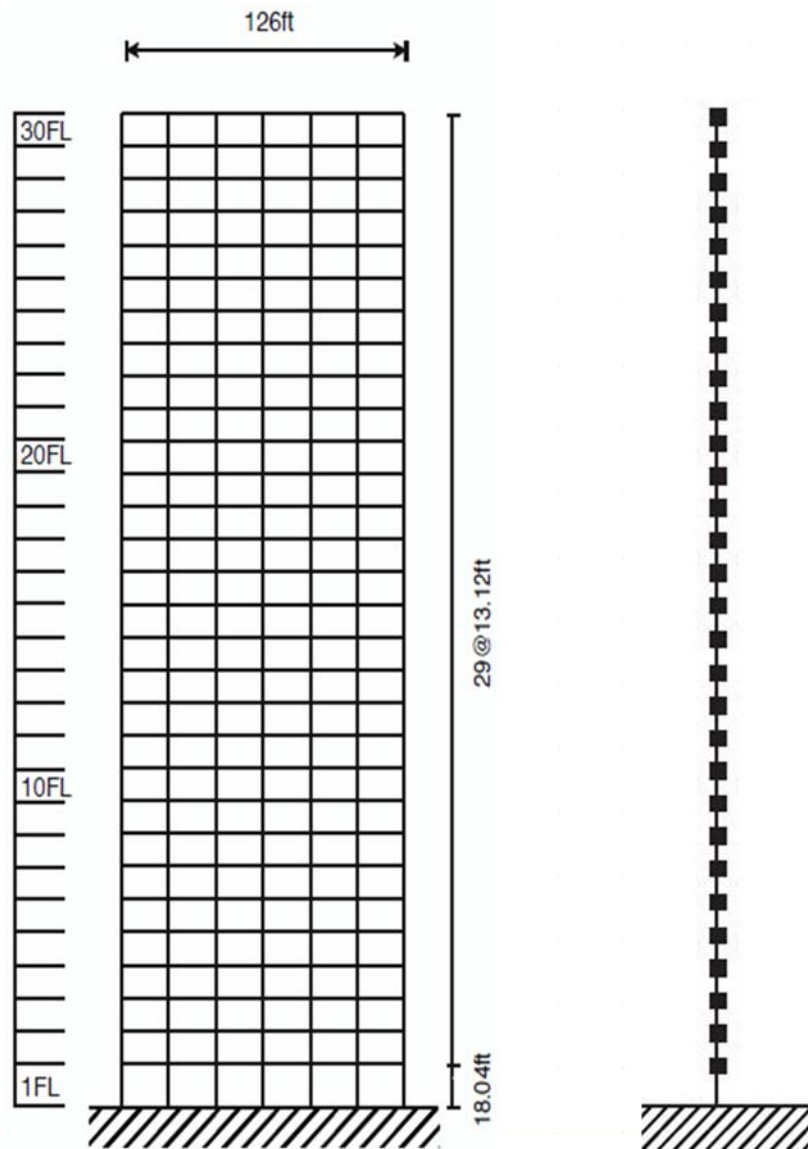


5-DOF Equivalent Model

$$W_{\text{tmd}} = 53 \text{ kip}$$
$$W_{\text{bldg}} = 0.849 * 450 \text{ kip}$$
$$f_{x1} = 1 \text{ Hz}$$
$$f_{y1} = 1.25 \text{ Hz}$$
$$f_{z1} = 11 \text{ Hz}$$

Analytical Substructure Parameters

Tall Building Model E



30-DOF Shear Building

$$W_{\text{tmd}} = 53 \text{ kip}$$

$$W_{\text{bldg}} = 63000 \text{ kip}$$

$$SF = 120$$

$$SL = \text{sqrt}(SF)$$

$$SI = SL^4$$

$$ST = \text{sqrt}(SL)$$

$$SV = SL/ST$$

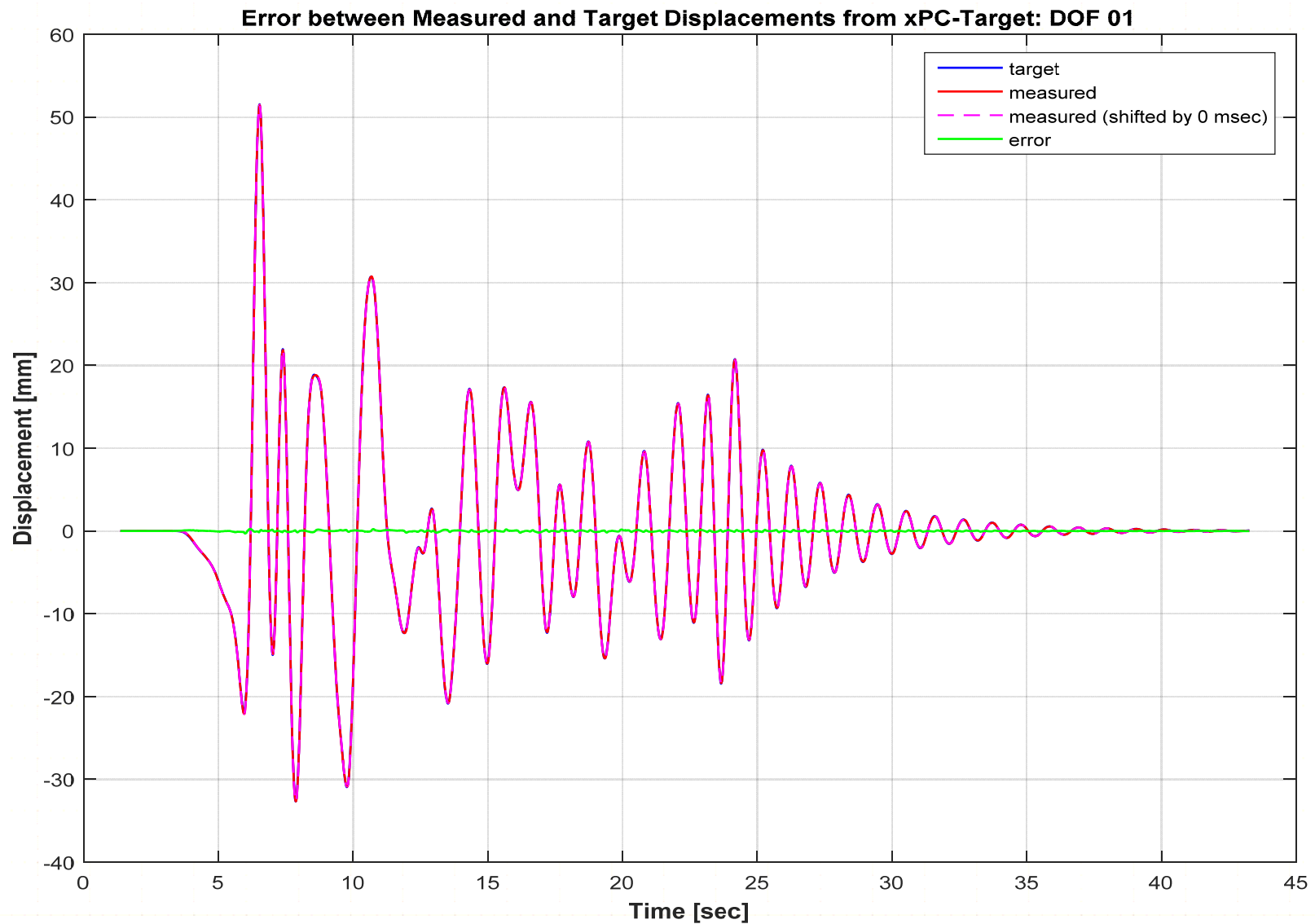
$$f_{x1} = 0.27 \text{ Hz}$$

$$T_{x1} = 3.7 \text{ sec}$$

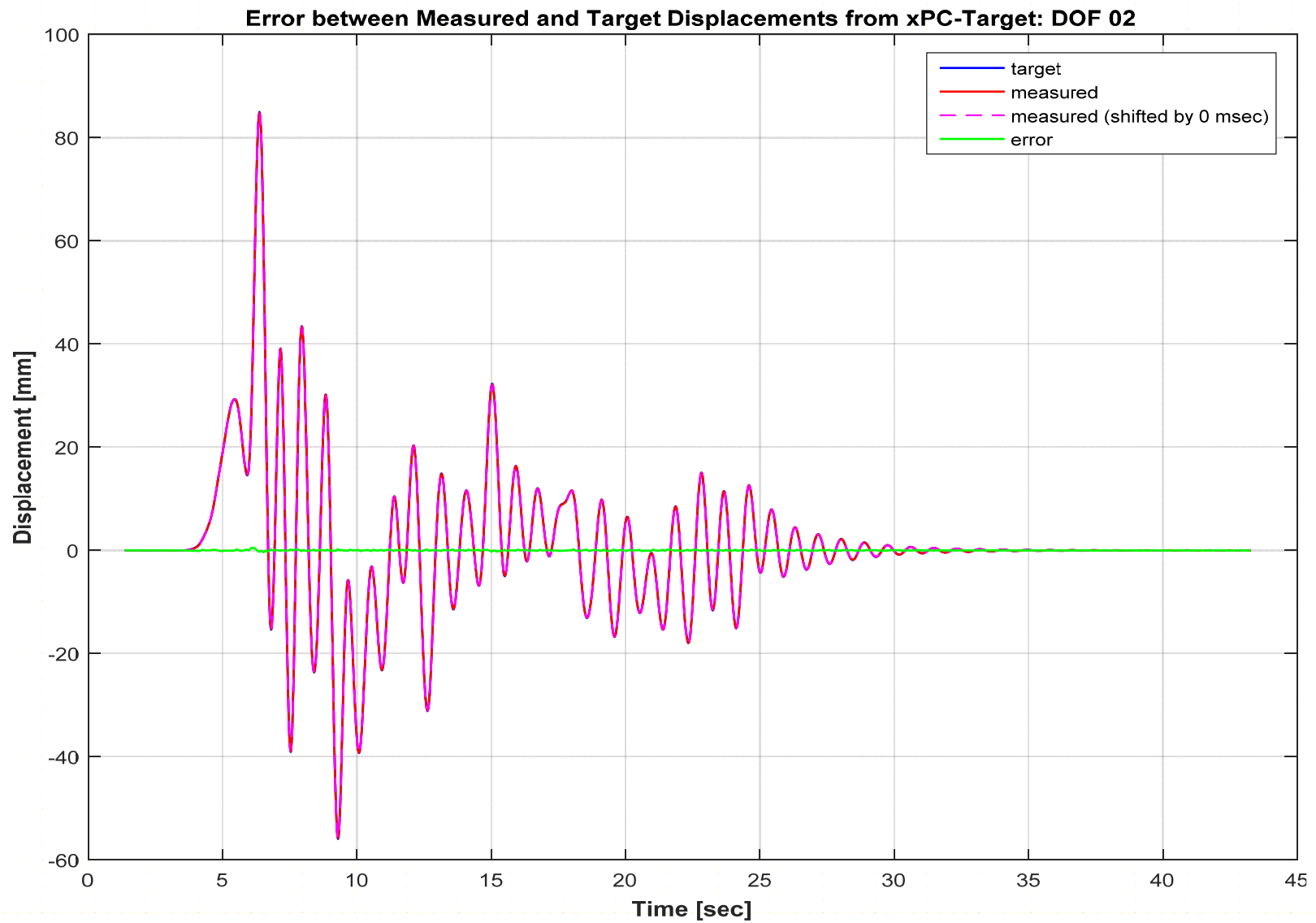
Movie of Test



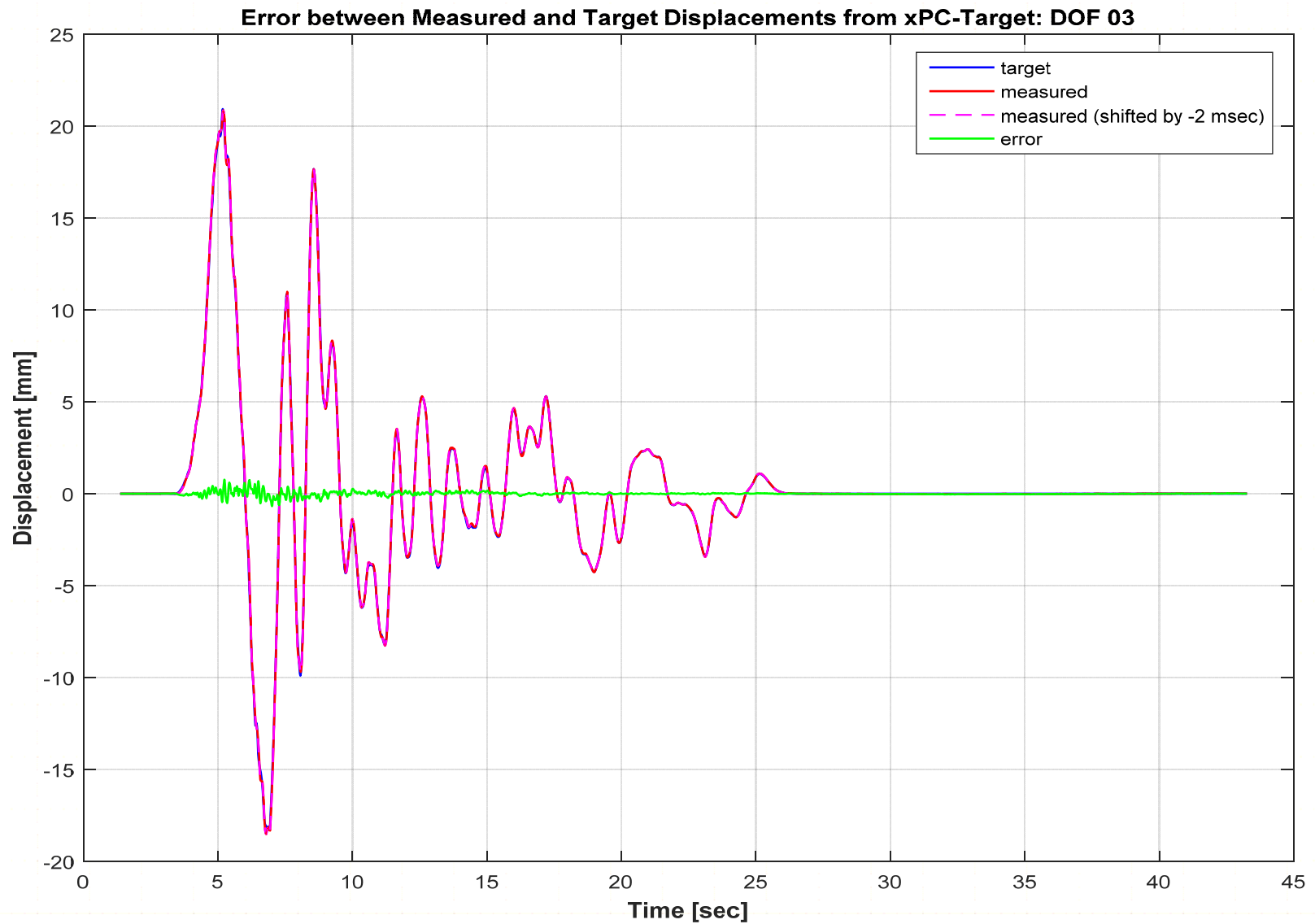
Delay Assessment



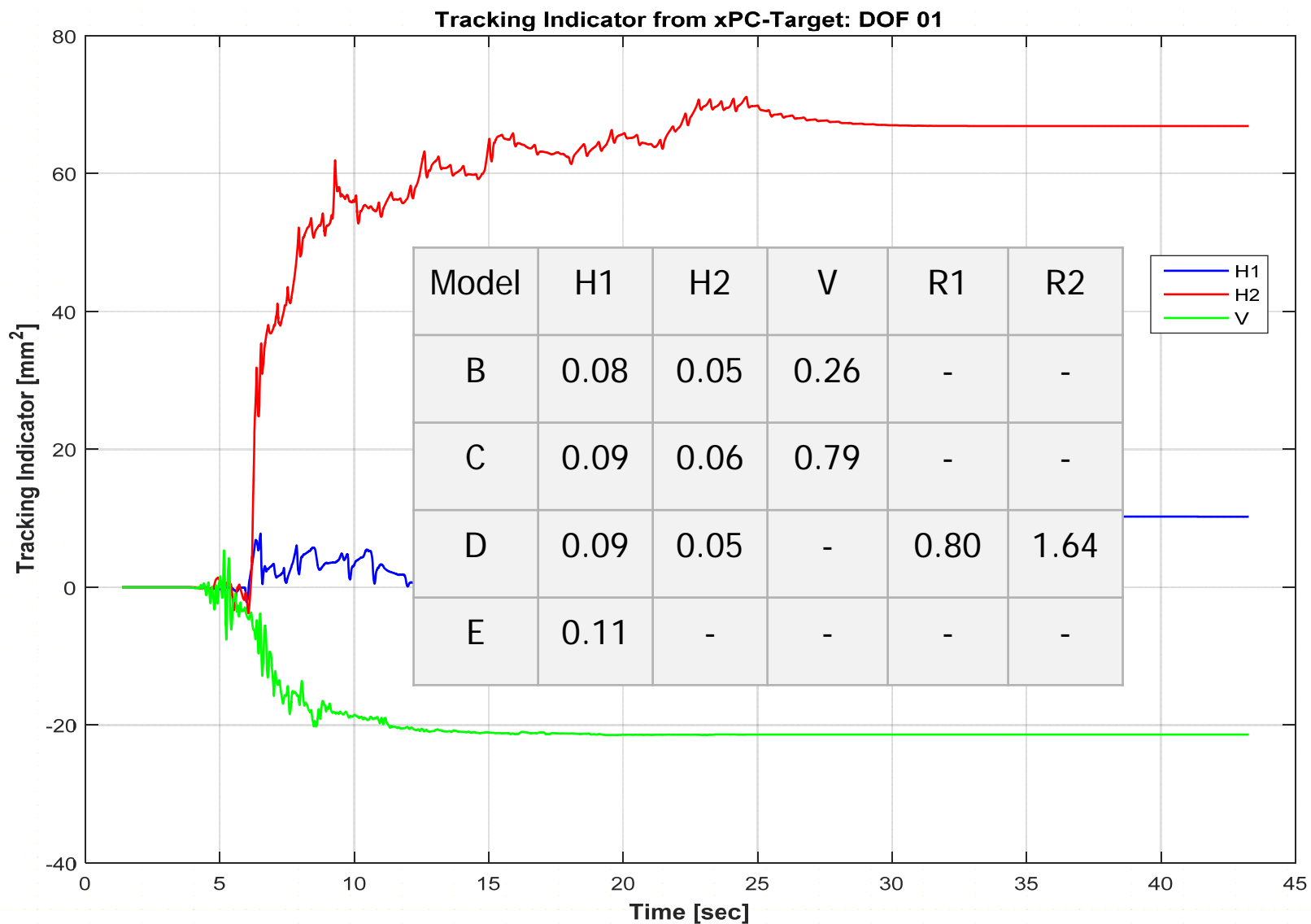
Delay Assessment



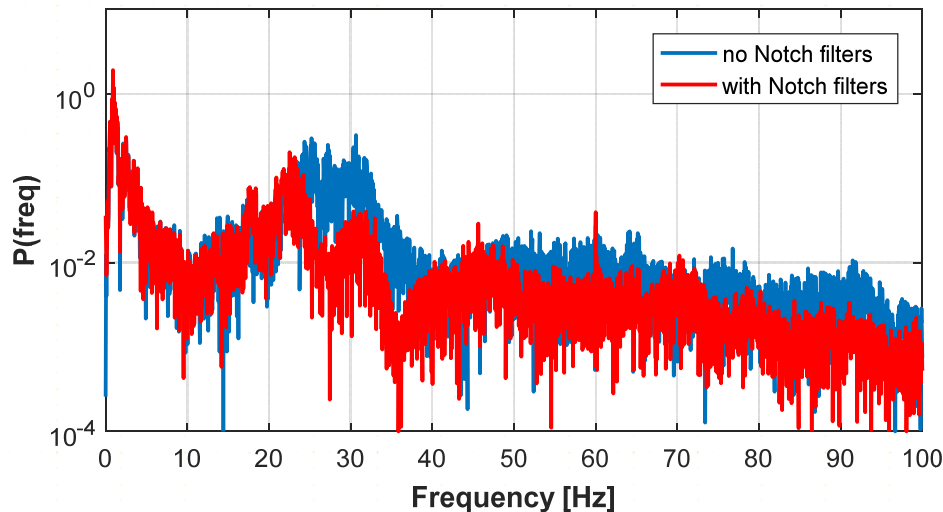
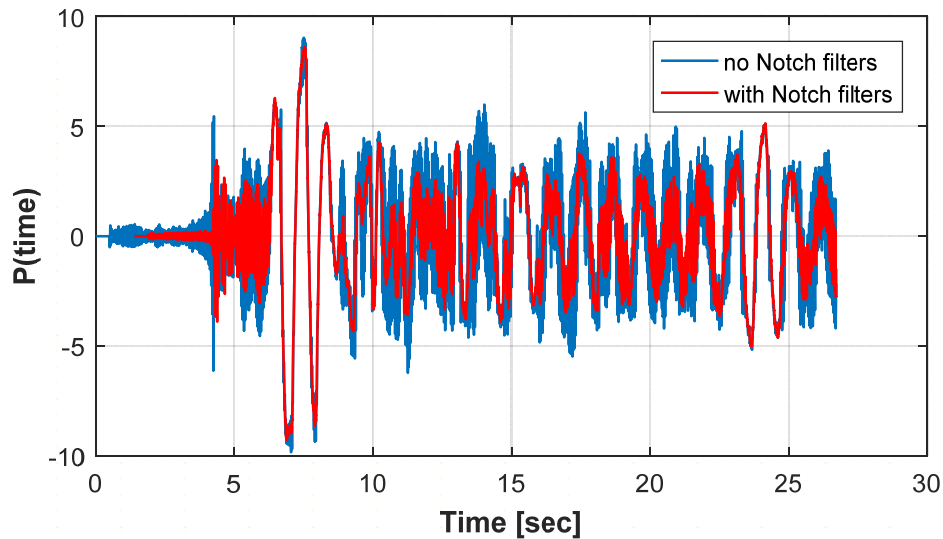
Delay Assessment



Tracking Indicator & NRMSE[%]



Filtering of Force Feedback



- Future work required
- Investigate other filtering techniques
- Investigate Kalman filtering techniques (can this be applied to force feedbacks using an predictive analysis model in parallel?)

Summary & Conclusions

- ★ Ability to drive a large scale shake table through a finite element model
- ★ Shake table platform can thus represent a floor or the roof of a building, the motion on top of a bridge column, or the ground surface on top of a soil domain
- ★ Ability to perform parameter studies
- ★ ATS delay compensator works very well

Summary & Conclusions

- ★ Use whenever the dynamics of the test specimen significantly affects the response of the supporting structure or soil and, therefore, alters the required input to the shake table as testing progresses
- ★ Need to further investigate sensor noise reduction methods to improve feedback signals (look into Kalman filters)

NEHRI@UCSD User Workshop
UC San Diego, December 12-13, 2016

Questions?
Thank you!

<http://openfresco.berkeley.edu>



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